Diffractive optic fluid shear stress sensor

Daniel W. Wilson, Jennifer A. Scalf, Siamak Forouhar, and Richard E. Muller

Jet Propulsion Laboratory, California Institute of Technology, MS 302-231, 4800 Oak Grove Drive, Pasadena, CA 91109 Tel: (818) 393-3548, Fax: (818) 393-4540, E-mail: daniel.w.wilson@jpl.nasa.gov

Frederic Taugwalder and Morteza Gharib

California Institute of Technology, M/C 205-45,1200 E. California Blvd., Pasadena, CA 91125 Tel: (818) 393-3548, Fax: (818) 393-4540, E-mail: mory@caltech.edu

Dominique Fourguette and Darius Modarress

VioSense Corporation, 2400 Lincoln Avenue, Altadena, CA 91001 Tel: (818) 393-3548, Fax: (818) 393-4540, E-mail: modarress@viosense.com

Abstract: Light scattering off particles flowing through a two-slit interference pattern can be used to measure the shear stress of the fluid. We have designed and fabricated a miniature diffractive optic sensor based on this principle.

©2000 Optical Society of America

OCIS codes: (170.3340) Laser Doppler velocimetry, (220.4000) Microstructure fabrication

1. Measurement concept

The goal of this sensor is to determine the shear stress of a fluid within the first few hundred microns from a wall. Within this region, the velocity gradient is linear, $u = \sigma y$, where u is the velocity, σ is the shear stress, and y is the vertical coordinate. Our diffractive optical micro-sensor generates a linearly diverging fringe pattern as illustrated in Fig. 1. The fringe spacing can be expressed as $\Delta = Ky$, where K is the slope of the first non-vertical fringe.

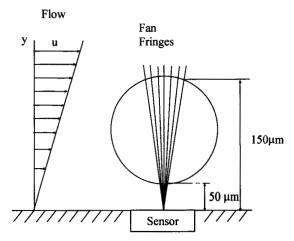


Figure 1. Schematic of the shear stress sensor principle.

As particles in the fluid flow through the linearly diverging fringes, they scatter light to a detector with a frequency f that is proportional to the velocity and inversely proportional to the fringe separation, $f = u/\Delta$. Using the relations for u and Δ above, the measured frequency is directly proportional to the wall shear,

$$f = \frac{\sigma y}{K y} = \frac{1}{K} \sigma$$

This technique was first presented by Naqwi and Reynolds using conventional optics [1]. A non-linearity of the velocity profile or the fringe pattern will translate into widening and skewness of the frequency distribution.

2. Design and modeling

A conceptual drawing of the micro shear stress sensor is shown in Figure 2. The diverging light from a diode laser is focused by a diffractive optical element (DOE) to two parallel line foci. These foci are coincident with two slits

in a metal mask on the opposite side of a quartz substrate. The light diffracts from the slits and interferes to form linearly diverging fringes to a good approximation. The light scattered by particles traveling through the fringe pattern is collected through a window in the metal mask. Another DOE on the backside focuses the light to an optical fiber connected to a detector.

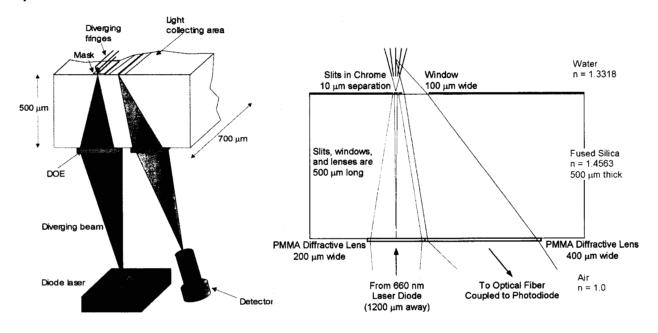


Figure 2. Schematic of the shear stress sensor assembly.

A series of simulations were performed to aid in the design of the sensor. A finite-difference simulation of the fringe pattern for 2 μ m wide slits separated by 10 μ m is shown in Figure 3. The fringe pattern displays a suitable number of fringes for adequate measurements. The number of high-contrast fringes is determined by the slit width and the divergence of the fringe pattern is determined by the slit separation.

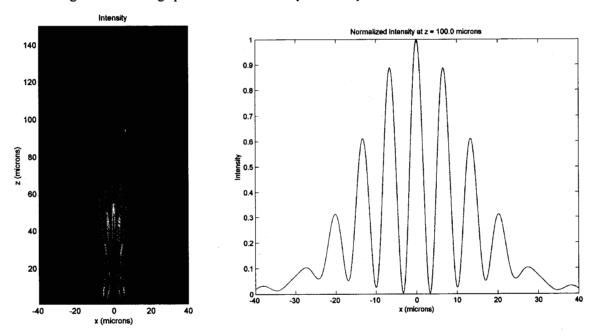


Figure 3. Fringe pattern resulting from 2 µm slits separated by 10 µm (propagation of a finite-difference solution of slit diffraction when illumined by the dual-line-focus laser lens).

3. Fabrication and testing

The main sensor element was fabricated by two-sided lithography on a 500 µm thick quartz substrate. The slits and collecting window on the front were fabricated by direct-write electron-beam lithography followed by wet etching of evaporated chrome. The polymethyl methacrylate (PMMA) diffractive optical elements on the back were fabricated by analog direct-write electron-beam lithography followed by acetone development [2]. A photograph and atomic force microscope scan of the dual-line focus-laser lens are shown in Fig. 4.

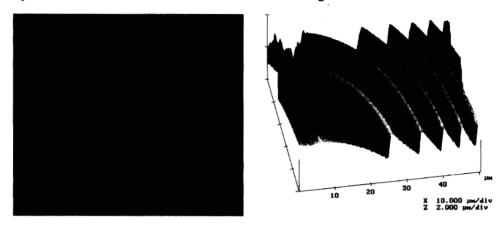


Figure 4. Photograph (left) and AFM scan (right) of the center of the dual-line-focus laser lens

The shear stress sensor's elements were assembled into a package (Fig. 5) with a diode laser (660 nm) and a port for the collection fiber. The overall size of this prototype is 15 mm in diameter and 20 mm in length. The fringes were imaged with a CCD camera using a microscope objective and are shown in Fig. 5. The fringe divergence was measured to be linear with a slope in close agreement with theory. The contrast is very satisfactory and preliminary tests using a moving surface through the fringe pattern yield a clear signal. Testing of the receiver side of the sensor element is underway.

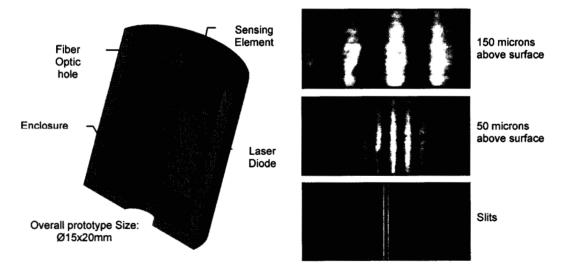


Figure 5. Shear stress sensor assembly (left) and photographs of the fringes at different heights above the surface (right).

4. References

- A. A. Naqwi and W. C. Reynolds, "Dual cylindrical wave laser-Doppler method for measurement of skin friction in fluid flow," Report No. TF-28, Stanford University (1987).
- [2] P. D. Maker, D. W. Wilson, and R. E. Muller, "Fabrication and performance of optical interconnect analog phase holograms made be E-beam lithography," in <u>Optoelectronic Interconnects and Packaging</u>, R. T. Chen and P. S. Guilfoyle, eds., Proc. SPIE CR62, 415-430 (1996).

Diffractive Optic Fluid Shear Stress Sensor

Daniel Wilson, Jennifer Scalf, Siamak Forouhar, Richard Muller Jet Propulsion Laboratory, California Institute of Technology Pasadena, California

Frederic Taugwalder and Morteza Gharib

California Institute of Technology

Pasadena, California

Dominique Fourguette and Darius Modarress

VioSense Corporation

Altadena, California











Wall Shear Principle

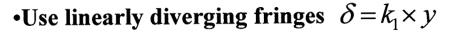
•Wall shear,
$$\sigma = \frac{\partial u}{\partial y}$$

•Velocity is linear near the wal($u \propto y$)

$$\sigma = \frac{u}{y}$$

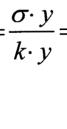
•Measured frequency proportional to U and the inverse of the local fringe separation, δ

$$f = u/\delta$$





$$f = \frac{\sigma \cdot y}{k \cdot y} = \frac{1}{k} \sigma$$













Flow

Fan Fringes

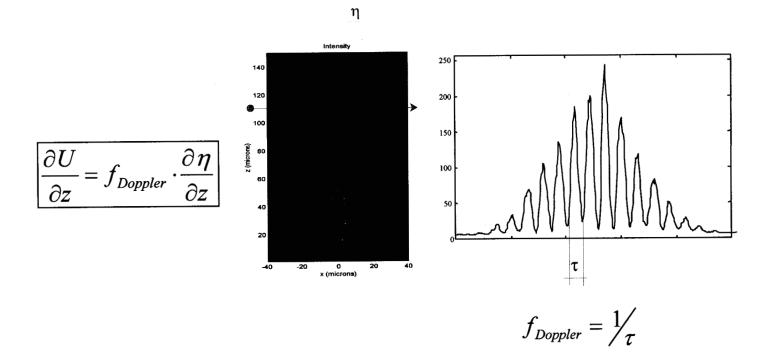
Sensor



150µm

50 µm

Wall Shear Principle







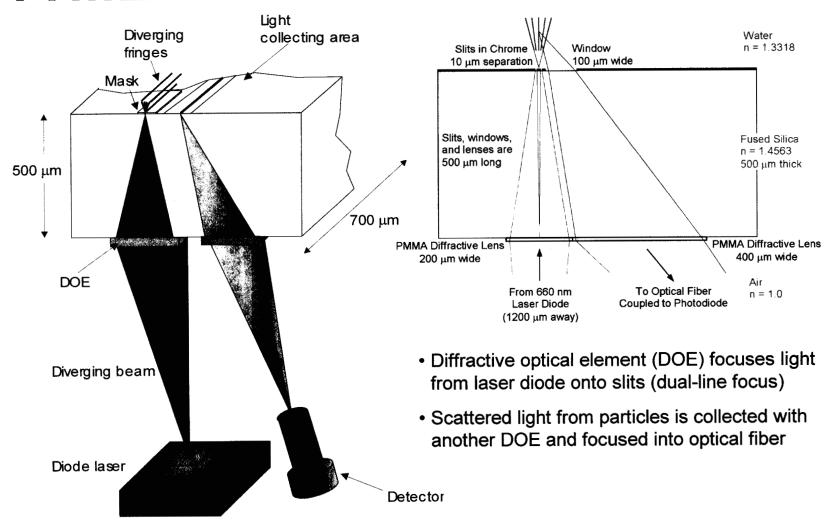








Shear Stress Sensor Design









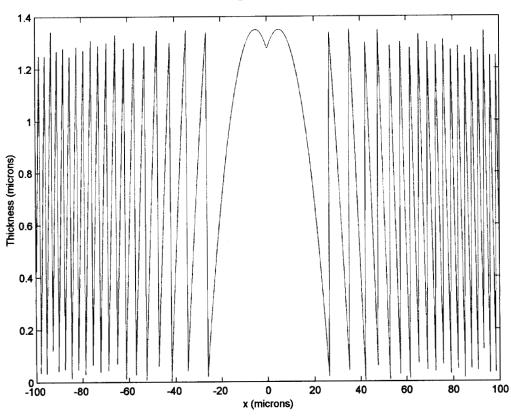






Shear Stress Sensor Modeling

Cross-section through dual-line-focus laser lens





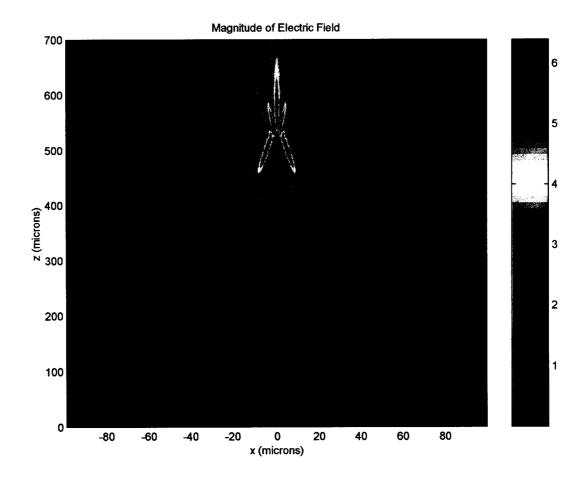








Laser Lens Focusing Simulation







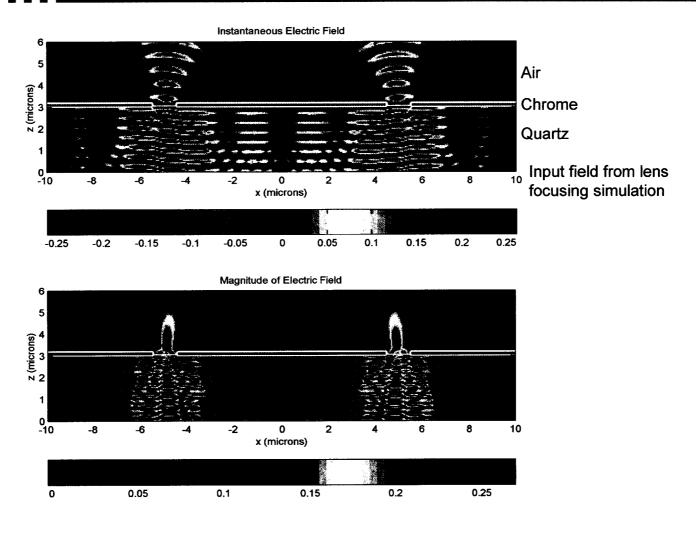






Propagation Through Slits Simulation

(Finite-Difference)







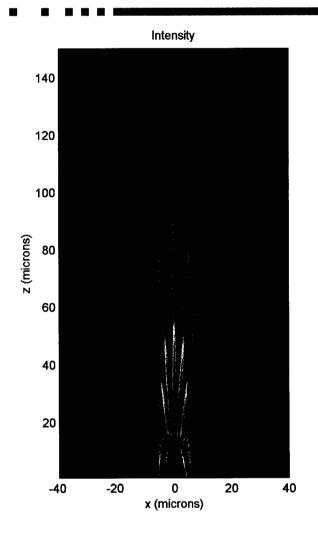


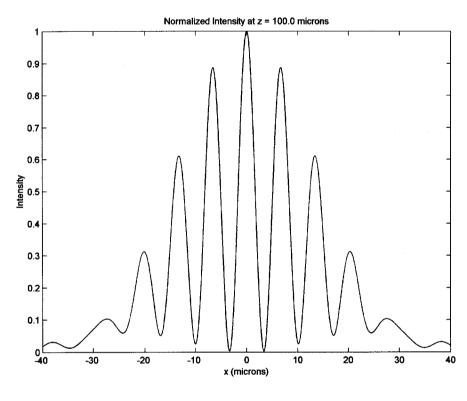






Measurement Volume Intensity for 2 μm Slits (Propagation of Finite-Difference Solution)









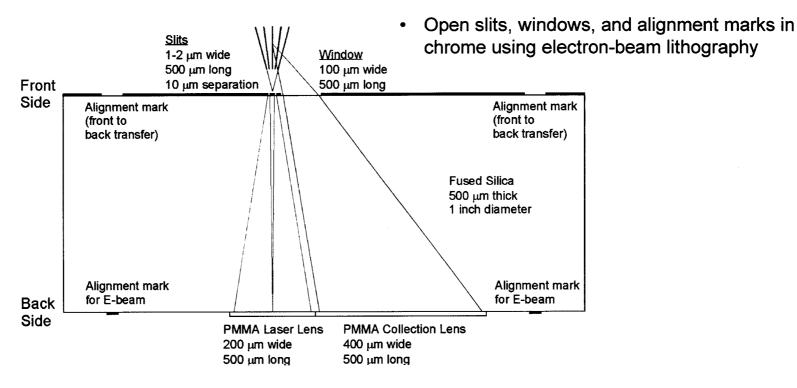








Shear Sensor Fabrication



- Define Ti/Pt alignment marks using optical lithography
- Fabricate diffractive lenses using analog directwrite electron-beam lithography

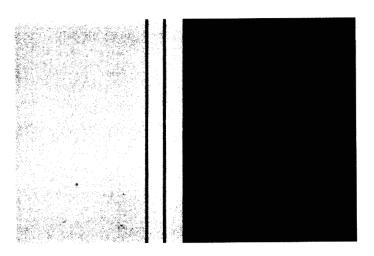




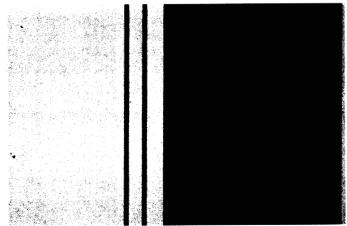




Front-Side Lithography on Chrome



1 μm slits 10 μm separation



2 μm slits 10 μm separation











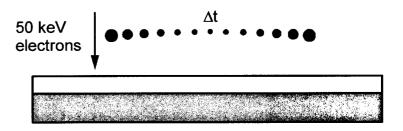
E-Beam Fabrication of Analog Diffractive Optics

Fabrication Method

- Thin film of polymethyl-methacrylate (PMMA - thin film Plexiglas) spun on substrate
- Direct-write analog-dose electron-beam lithography using JEOL JBX-5DII (50 kV)
- Electron beam breaks bonds in the PMMA increases solubility in acetone
- Acetone etches exposed PMMA to produce surface relief pattern

Thin film of PMMA on substrate material





Advantages

- Well controlled analog depth (< 5% error)
- Arbitrary patterns
- No pattern misalignment
- Prototype elements are easily fabricated

After acetone development





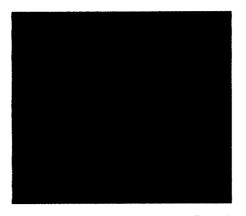




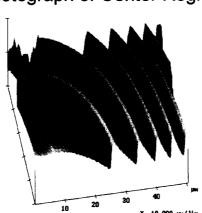




Dual-Line-Focus Laser Lens



Photograph of Center Region



Section Analysis 0-1-0 25.0 50.0



AFM Profile of Surface





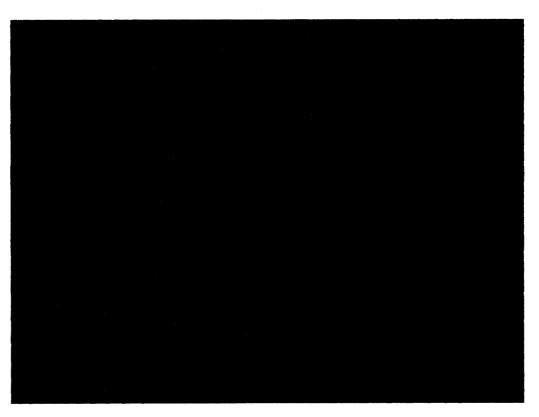






1.443 рм

Collection Lens



Photograph of Center Region



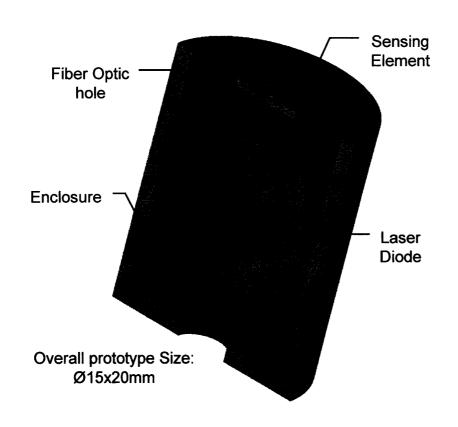


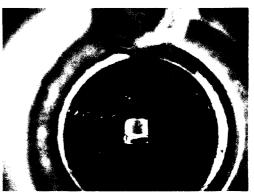






Packaging











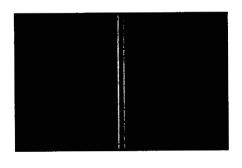




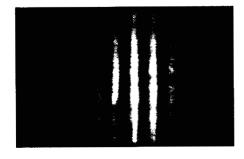


Fringe Pattern Images

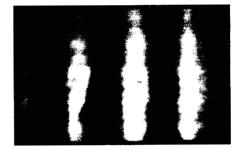
- 2 micron slits separated by 10 microns
- Interference fringes at 50 and 150 microns



Slits



50μm from surface



150μm from surface



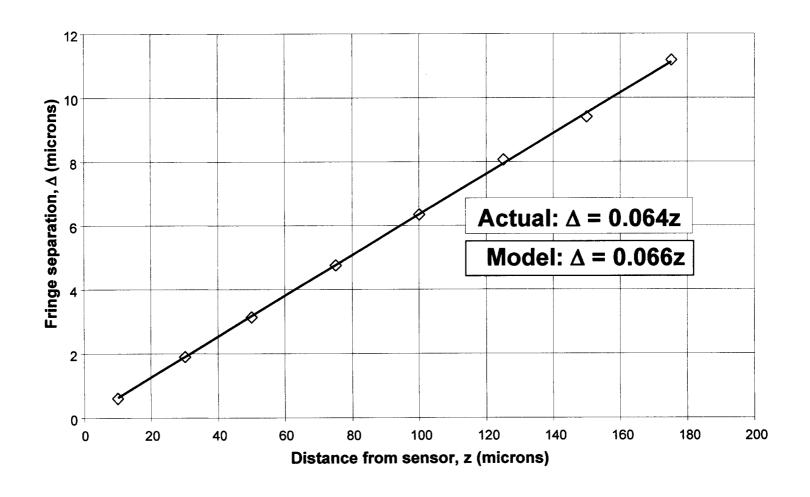








Measured Fringe Separation





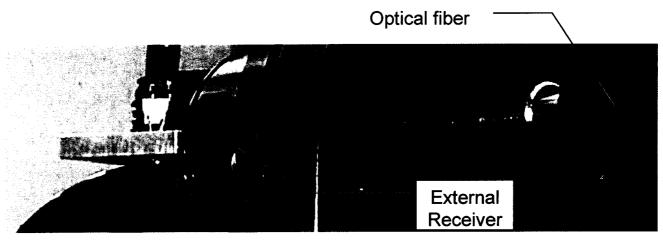


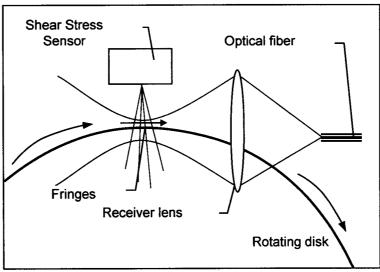






Shear Stress Sensor Test Setup







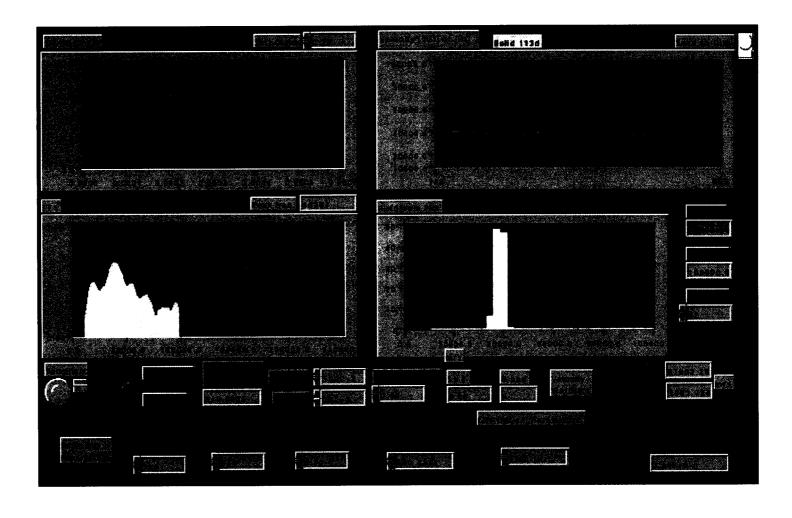








Signal with External Receiver











Conclusion

- Designed a non-invasive fluid shear stress sensor
- Utilized a two-sided fabrication technique to realize the diffractive optic sensor head.
- Tested the emitter side of the sensor and obtained good agreement with the model
- Future work will include improvement of emitter/receiver isolation and integration of the receiver fiber.







